Combustion Synthesis of Mullite/Metal Boride Composites

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Abstract

Formation of composite materials composed of mullite (3Al₂O₃·2SiO₂) and transition metal borides (NbB₂ and TaB₂) was studied by self-propagating high-temperature synthesis (SHS). Starting materials included not only metal oxides (Nb₂O₅ and Ta₂O₅) and boron oxide (B_2O_3) as the sources of metallic elements and boron, but also Al and Si powders as the reducing agents. The evolution of mullite from in situ formed SiO₂ and Al₂O₃ and synthesis of NbB₂ and TaB₂ were investigated. The effect of excess Si addition was studied on the combustion temperature, flame-front propagation velocity, and phase composition of the final product. For formation of the NbB₂/mullite composites, the combustion velocity about 2.5 mm/s and reaction temperature around 1500 °C decreased slightly as the Si content increased. However, a considerable decrease in combustion front velocity from 2.74 to 1.43 mm/s and in reaction temperature from 1600 to 1250 °C was observed for the production of the TaB₂/mullite composites. The XRD patterns of the final products confirmed the role of excess Si in the improvement of silicothermic reduction of B_2O_3 and subsequent evolution of NbB₂, TaB₂, and mullite. The EDS analysis indicated an atomic proportion close to that of 3Al₂O₃·2SiO₂ for the mullite grains synthesized in this study.

Keywords: combustion synthesis, mullite, transition metal borides, XRD, SEM

1. Introduction

Mullite composites have attracted great attention due to the broadness of their industrial applications. Mullite with stoichiometries ranging from relatively silica-rich $3Al_2O_3 \cdot 2SiO_2$ (3:2 mullite) to alumina-rich $2Al_2O_3 \cdot SiO_2$ (2:1 mullite) is the only stable crystalline phase in the aluminosilicate system [1]. For further improved fracture toughness, flexural strength, and ther-

mal shock resistance, mullite-based composites containing ZrO₂ and Al₂O₃ were extensively studied [2-3]. Lately, other ceramic additives such as TiC and TiB₂ have gained increasing attention [4-5]. A variety of processing techniques with different starting materials have been employed to prepare mullite in either monolithic or composite forms, and they include the sol-gel method, reaction sintering, spark plasma sintering, solution combustion synthesis, self-propagating high-temperature synthesis (SHS), and thermal explosion. The SHS method takes advantage of highly exothermic reactions, and has the merits of low energy requirement, short processing time, simplicity, high productivity, and structural and functional diversity of final products [6-7]. In addition to the yield of Al₂O₃, high exothermicity of the thermite reaction is a great benefit for the SHS process. Therefore, the thermite-based SHS technique has been utilized to prepare mullite combined with ceramic or intermetallic phases.

This study aims to fabricate NbB₂/mullite and TaB₂/ mullite composites by combustion synthesis in the SHS mode. The SHS process involves coreduction of metal oxides (Nb₂O₅ and Ta₂O₅) and B₂O₃ by Al and Si. Due to the evaporation loss of Si at elevated temperatures, the effect of excess Si addition was studied on the combustion temperature, flame-front velocity and phase composition.

2. Method

The starting materials of this study include Nb₂O₅ (Strem Chemicals, < 45 μ m, 99.9%), Ta₂O₅ (Alfa Aesar, < 45 μ m, 99.85%), B₂O₃ (Strem Chemicals, 99.9%), Al (Showa Chemical Co., < 45 μ m, 99.9%), and Si (Strem Chemicals, < 45 μ m, 99%). The reactant mixtures were formulated as 13/11Nb₂O₅ (or Ta₂O₅) + 26/11B₂O₃ + 6Al + (2x)Si with x = 1.0–2.0 for studying the effect of excess Si (x > 1.0) addition.

Sample compacts were prepared in a cylindrical shape with 7 mm in diameter, 12 mm in length, and 50% in relative density by compressing the well-mixed reactant powders. Combustion experiments were performed under high-purity (99.99%) argon of 0.15 MPa. The combustion propagation rate and reaction temperature were precisely measured. Details of the experimental setup and technique were reported elsewhere [8].

3. Results and Discussion

A typical combustion sequence illustrated in Fig. 1 is associated with formation of TaB₂/mullite from a powder compact with x = 1.0. It is evident that upon ignition the combustion front was readily formed and propagated progressively along the sample, confirming sufficiency of the reaction exothermicity.



Fig. 1 A sequence of self-sustaining combustion wave

For the formation of the NbB₂/mullite composite, the combustion velocity of about 2.5 mm/s and reaction temperature of around 1500 °C decreased slightly as the Si content exceeded the stoichiometric amount. This implies a reduction in the reaction exothermicity, because the endothermic mullitization process is enhanced. However, a considerable decrease in combustion front velocity from 2.74 to 1.43 mm/s and in reaction temperature from 1600 to 1250 °C was observed for the production of the TaB₂/ mullite composites. This was attributed to the yield of TaSi₂ a lower exothermic phase in comparison to TaB₂. In contrast, no silicide phases existed in the NbB₂/mullite composite.

Besides mullite, niobium borides of three phases, NbB, Nb₃B₄, and NbB₂, were identified in the final product. The presence of NbB and Nb₃B₄ as the minor phases means a deficiency of boron. This was probably caused by lack of sufficient Si to fully carry out metallothermic reduction of B₂O₃. For the reactant compact with excess Si of x = 2.0, both NbB and Nb₃B₄ are considerably reduced.

The XRD pattern of the product synthesized from an exactly stoichiometric sample is shown in Fig. 2(a). First of all, the evolution of mullite from in situ formed SiO₂ and Al₂O₃ was achieved and TaB₂ was identified as the dominant boride phase, confirming coreduction of Ta₂O₅ and B₂O₃ by both Al and Si. However, the presence of free Al_2O_3 means that the evaporation loss of Si brings about a shortage of SiO₂. The lack of Si correspondingly caused incomplete reduction of Ta_2O_5 and B_2O_3 . For the Si-excess samples of x = 1.5 and 2.0, Fig. 2(b) and (c) show almost no free Al₂O₃ and a slight decrease in TaB for the resulting products. This implies that the degree of silicothermic reduction of B₂O₃ was enhanced. However, excess Si considerably increased the amount of TaSi₂, indicative of lack of boron for the formation of TaB₂.



Fig. 2 XRD patterns of TaB₂/mullite synthesized from samples with Si of (a) x = 1.0, (b) x = 1.5, and (c) x = 2.0



Fig. 3 SEM micrograph and EDS spectrum of $NbB_2/mullite$ synthesized from a sample of x = 1.5

The typical microstructure of fracture surface of the NbB₂/mullite composite synthesized from a sample of with x = 1.5 is displayed in Fig. 3. For those plate-like grains formed into a structure with rectangular opens, the EDS analysis advises their atomic proportion of O:A1:Si = 63.09:28.05:8.86, which matches closely with that of 3:2 mullite. The other constituent NbB₂ exists as fine particles distributed over thin mullite plates.

4. Conclusions

Preparation of NbB₂/mullite and TaB₂/mullite was conducted by combustion synthesis in the SHS mode involving metallothermic reduction of Nb₂O₅, Ta₂O₅, and B₂O₃. Combustion of the sample adopting two reducing agents (Al and Si) was more exothermic and speedy than that with pre-added SiO₂ and using Al as the only reductant. It was found that the Si content about 50 mol% in excess of the stoichiometric quantity was required by the Si-containing samples to facilitate the silicothermic reduction of B_2O_3 to the utmost extent. As a result, the formation of NbB_2 or TaB_2 and mullite was improved. The mullite grains synthesized in this study showed an atomic proportion close to that of 3Al₂O₃·2SiO₂. In conclusion, the advantages of utilizing two reductants include more exothermic combustion, higher self-sustainability, shorter reaction time, and better phase transformation.

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