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# **Comprehensive Review of Natural Convection Heat Transfer in Annulus Complex Enclosures**

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#### ABSTRACT

The natural convection heat transfer has many applications in engineering like solar collectors, cooling of electronic equipment, and geothermal engineering. The present work demonstrates the recent publications in the last ten years in this specific subject for a body located in complex shapes like rhombic, wavy, trapezoidal, elliptical, and Parallelogrammic enclosure. Many parameters like Ra, Nu, number of undulations, the position of the inner body had been addressed and discussed to draw the main conclusions and recommendations. It is worthy to mention that a wavy enclosure has been investigated less than the other simple enclosure shapes due to its complexity. Besides that entropy generation should be included in future studies in complex shapes of enclosure as this will helps the researchers to extend their studies. The inner bodies inside trapezoidal, parallelogrammic enclosure are very limited, and more investigation should be done. The review concluded for the different shapes of enclosure with the tables that illustrate the major finding of each study. Finally, the governing equations of the natural convection of enclosure filled with pure fluid, porous medium, and nanofluid had been addressed.

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# 1. Simple Enclosures

The natural convection heat transfer in simple enclosure shapes as illustrated in **Fig. 1** had been studied numerically by various researchers due to its importance in energy related applications. Some of these studies were [1-20]. Ghasemi et al. [2] investigated numerically the influence of the magnetic field on buoyancy driven fluid flow in a square nanofluid enclosure filled with  $Al_2O_3$ -water. The results indicated that Rayleigh and Hartmann number had an opposite influence on heat transfer while the increasing of nanoparticle loading helps in augmentation of heat transfer.

Another important study focus on using a different model of nanofluid properties presented by Lai and Yang [3] using Lattice-Boltzmann scheme. They found that different methods of nanofluid properties affect the Nusselt number value. Bhuvaneswari et al. [4] computed using a finite volume approach the natural convection with the magnetic field in a square enclosure. The major of this study is that the authors applied sinusoidal temperature distribution to both of the sidewalls and keeping the horizontal wall adiabatic. The results indicated that increasing Hartmann number

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researchers

reduces the heat transfer. Alam et al. [5] demonstrated the impact of aspect ratio and heat source power density on fluid flow circulation and heat transfer of free convection within rectangular enclosure heated and cooled partially from the vertical walls while the rest of them and others walls maintained adiabatic. They found that increases the aspect ratio augmented the heat transfer and it reaches its maximum value at aspect ratio equals to one. [6, 7] illustrated the double diffusive natural convection in tilted rectangular enclosure including the impact of a magnetic field and heat source. They concluded that heat source had a crucial impact on heat transfer. For more details about the previous works, the reader can be referring to [8-15]. Wang et al. [16] presented a comparison between the impact of Al<sub>2</sub>O<sub>3</sub>-H<sub>2</sub>O and Ga-H<sub>2</sub>O and the radius under different Rayleigh numbers of heat transfer using a two-phase lattice Boltzmann method. The authors deduced that Ga-H<sub>2</sub>O enhances the heat transfer better than Al<sub>2</sub>O<sub>3</sub>-H<sub>2</sub>O. Al-Farhany and Abdulkadhim [17] examined the conjugate problem in a square enclosure filled with porous media under various Rayleigh and Darcy numbers and they obtained that wall thickness effects on the transformation of the heat mode from convection into conduction which reduces the heat transfer. Barik and Al-Farhany [21] studied the inflleucne of inclined baffle in nanofluid/porous square enclosure using COMSOL. Dutta et al. [18] studied the entropy generation in quadrant porous enclosure heated sinusoidally from its bottom wall. They concluded that entropy generation due to fluid friction is dominated at high values of Darcy number while they noticed the entropy formed due to heat transfer is the major influencer on low Darcy number. Torki and Etesami [19] experimentally studied the natural convection of a rectangular enclosure filled with SiO2 at different nanofluid loading and enclosure inclination angles. They obtained that the nanofluid did not affect low concentration value and the inclination angle of a rectangular enclosure had a strong effect. In addition, the Nusselt number is increased as the inclination angle goes up. Graževičius et al. [20] studied experimentally and numerically using ANSYS 17.2 of natural convection for removing heat from the reactor using a passive system. Also, the natural convection in complex shapes had been reported by various researchers like [22-25].



Figure 1. Schematic diagram of simple shape of enclosure (square) [2]

Sheikholeslami and Chamkha [22] examined the free convection in a liddriven enclosure filled with  $Fe_3O_4$  with applied magnetic field and wavy wall. They obtained that increasing magnetic number, Rayleigh number, and nanofluid volume fraction increases the Nusselt number while Hartmann number had a reverse impact on Nusselt number. Sheikholeslami [23] studied the liquid metal due to natural convection in a wavy enclosure for various values of Rayleigh number, amplitude of wavy wall, and Hartmann number. It is worthy to mention here that the last parameters increasing lead to reduce the Nusselt number. Two important studies collect

Besides that, various researchers dealt with the different shapes of an inner body located inside a regular simple enclosure shape like a square or rectangle that had been presented in Fig. 2. The inner body located within the enclosure had a wide range of applications like a solar collector, fuel cell, etc. The researchers among the world interested in understanding the effect of inner shapes like circular, triangular, elliptical, and wavy inside different shapes of the enclosure. Other researchers focus on the position of the inner body and change the direction vertically, horizontally and longitudinally. These are the main parameters that affect the heat transfer so that some of these studies are presented by [26-31]. Lee et al. [26] used an immersed boundary method to examine the changing of an inner cylinder located within square enclosure horizontally and longitudinally while another study by [27, 28] illustrates the vertical position on heat transfer. Ali et al. [29] studied the mixed convection due to rotating inner circular cylinder within square enclosure filled with air using ANSYS FLUENT. Roslan et al. [30] studied the heated circular cylinder located within the cold enclosure. The main important thing in this study is that the inner circular cylinder had sinusoidal temperature under unsteady conditions. We summarized the previous publications regarding the natural convection within simple shape, complex shapes and simple annulus enclosure in Table 1-3, respectively.

between MHD and wavy enclosure is presented in [24, 25] and they agreed

with the previous mentioned results in the previous works of various

Finally, the present work concentrates on the inner body located inside the non-square enclosure.



Figure 2. Schematic diagram of the inner body within simple enclosure shape [27]

| Ref                  | Objective                | Enclosure shape    | Software/model used | Conclusions                   | Special findings                 |
|----------------------|--------------------------|--------------------|---------------------|-------------------------------|----------------------------------|
| Ghasemi et al. [2]   | MHD and nanofluid        | Square             | CVM using SIMPLE    | Hartmann and Rayleigh         | Nanofluid effect may increases   |
|                      | effect                   |                    | algorithm           | numbers had an inverse        | of decreases Nusselt number      |
|                      |                          |                    |                     | effect on Nusselt number      | depending upon Rayleigh          |
|                      |                          |                    |                     |                               | number                           |
| Lai and Yang [3]     | Al2O3 nanofluid          | Square             | Lattice – Boltzmann | Nanofluid thermophysical      | LBM is recommended for the       |
|                      |                          |                    | method (LBM)        | models effect on the          | practical engineering            |
|                      |                          |                    |                     | computation of the Nusselt    | applications                     |
|                      |                          |                    |                     | number                        |                                  |
| Bhuvaneswari et      | Sinusoidal temperature   | Square             | FVM                 | Increasing Hartmann           | The phase deviation of applied   |
| al. [4]              | boundary conditions      |                    |                     | number reduces the heat       | Sinusoidal temperature effect    |
|                      | with MHD effect          |                    |                     | transfer                      | on Nusselt number                |
| Alam et al [5]       | Partial cooling/heating  | Rectangle          | FEM                 | Nussselt number increases     | The maximum Nusselt number       |
|                      | and aspect ratio         |                    |                     | when the aspect ratio range   | is achieved at aspect ratio      |
|                      |                          |                    |                     | from $0.5 - 10$ beyond this   | equals to one.                   |
|                      |                          |                    |                     | value it reduces Nu as it     |                                  |
|                      |                          |                    |                     | goes up.                      |                                  |
| Teamah et al. [6]    | Double diffusive,        | Inclined rectangle | CVM SIMPLER         | Lowest and Highest value      | Sherwood number is not           |
|                      | Inclinations angle,      |                    | algorithm           | of Sherwood and Nu            | affected by heat absorption and  |
|                      | MHD, buoyancy ratio      |                    |                     | numbers were at 75 and 150    | generation.                      |
| El Qarnia et al. [9] | Phase change due to      | Rectangle          | FVM/FORTRAN         | Two correlations had been     | The developed model can be       |
|                      | melting                  |                    |                     | developed.                    | used in phase change material    |
| Nithyadevi et al.    | Effect of numbers of     | Rectangle          | FVM                 | Increasing numbers of         | Increasing heat generation       |
| [15]                 | discrete heater, Prandtl |                    |                     | heater and Prandtl number     | reduces the heat transfer        |
|                      | number and heat          |                    |                     | enhance the heat transfer     |                                  |
|                      | generation               |                    |                     |                               |                                  |
| Qi at a;. [16]       | Ra and nanofluid radius  | Rectangle          | Two-phase LBM       | Small radius of nanofluid     | The augmentation of nanofluid    |
|                      |                          |                    |                     | can enhance better than the   | is better at low Ra number       |
|                      |                          |                    |                     | big size                      |                                  |
| Al-Farhany and       | Conjugate problem in     | square             | FEM/COMSOL          | Increasing Ra and Da          | Increasing the conduction wall   |
| Abdulkadhim [17]     | porous medium            |                    |                     | enhance the heat transfer     | reduces the heat transfer        |
| Dutta et al. [18]    | Porous media, entropy    | Quadrant           | FEM                 | Increasing Ra and Da          | When the Darcy number is         |
|                      | generation with non-     |                    |                     | increase the heat transfer as | low, the heat transfer's entropy |
|                      | uniform bottom wall      |                    |                     | mentioned in most of the      | generation is higher while at    |
|                      | temperature              |                    |                     | publications                  | the high Da, the entropy         |
|                      |                          |                    |                     |                               | generation due to friction of    |
|                      |                          |                    |                     |                               | fluids is higher                 |
| Torki et al. [19]    | nanofluid, inclined      | Rectangle          | Experimental study  | Increasing Rayleigh number    | Inclination effect is higher at  |
|                      | enclosure                |                    |                     | increases Nu                  | low nanofluid loading            |

### Table 1 summarized the studies of natural convection inside a simple shape of enclosure

Table 2 summarized the studies of natural convection inside the complex shape of enclosure

| Ref                           | Objective                                  | Enclosure shape | Software/model used | Conclusions  | Special findings   |
|-------------------------------|--|-----------------|---------------------|--|--|
| Sheikholeslami<br>et al. [22] | MHD, lid-driven<br>cavity, ferro nanofluid | Wavy            | FEM/FORTRAN         | Increasing nanofluid<br>loading, Rayleigh, and<br>magnetic numbers<br>increases the heat<br>transfer while Hartmann<br>increases to reduce it. | The authors studied the<br>wavy top wall which is a<br>little bit make a difference<br>with the previous<br>publications |
| Sheikholeslami<br>et al. [23] | MHD  | Wavy            | CVFEM               | Increasing Hartmann<br>number reduces Nu   | Hartmann number is highly<br>effects on fluid flow and<br>heat transfer  |
| Xiong, et al.<br>[25]         | Nanofluid/porous<br>layers and MHD         | Wavy            | CVFEM               | Ha increasing leads to<br>reduction in the Nusselt<br>number   | Increasing Da leads to an<br>improvement in the heat<br>transfer   |

| Ref              | Objective                  | Enclosure shape         | Software/model used        | Conclusions                   | Special findings                   |
|------------------|----------------------------|-------------------------|----------------------------|-------------------------------|------------------------------------|
| Lee et al. [26]  | Position of inner circular | Circular cylinder       | FVM                        | Increasing Ra number leads    | It is noted that when the          |
|                  | cylinder in horizontal and | within square           |                            | to enhance the Nusselt        | cylinder becomes closest to the    |
|                  | diagonal direction         | enclosure               |                            | number                        | corner or left walls, the eddies   |
|                  |                            |                         |                            |                               | that located in the direction of   |
|                  |                            |                         |                            |                               | the cylinder will be separated     |
|                  |                            |                         |                            |                               | while one large eddies formed      |
|                  |                            |                         |                            |                               | behind the cylinder                |
| Hussain and      | Vertical position of the   | Circular cylinder       | FVM                        | As Ra increases, Nu goes      | When the cylinder moves            |
| Husssein [27]    | inner cylinder, constant   | within square           |                            | up                            | vertically upward, two inner       |
|                  | heat flux is considered    | enclosure               |                            |                               | cells (eddies) are formed below    |
|                  | for the cylinder           |                         |                            |                               | it.                                |
| Park et al. [28] | Same the study of [27] ex  | cept they applied isoth | erm hot temperature to the | cylinder                      |                                    |
| [30] and [31]    | Unsteady case study        | Wavy temperature        | COMSOL                     | Increasing the oscillation of | The frequency of wavy              |
|                  |                            | conditions inside a     |                            | the heat source leads to      | condition $25\pi - 30\pi$ augments |
|                  |                            | square cavity           |                            | improve the heat transfer.    | the heat transfer better           |

Table 3 summarized the studies of natural convection between inner body within regular (simple) enclosure shapes

#### 2. Triangular enclosure

This section describes different shapes of an inner body located inside a triangular enclosure. Schematic diagram of this case study is illustrated below in **Fig. 3**. Some of these studies presented by [32-38].





Xu et al. [32] examined numerically the natural convection heat transfer between various shapes of the inner cylinder (circular, square, rhombic, and triangular) located inside the triangular enclosure tilted for various inclination angle. The inner cylinder is kept at uniform hot temperature while the triangular enclosure is cold. The governing equations had been solved numerically using a finite volume method and validated with the previously published work along the bottom wall. The results are crucial and indicate that increasing the Rayleigh numbers breaking down the symmetry of streamlines contours and concentrates the isotherms contours to the top between the gaps. Yu et al. [33] examined the influence of various values of Prandtl number on heat transfer between a circular cylinder located inside an inclined triangular enclosure. The equations of mass, energy, and momentum of fluid along with Boussinesq approximations had been solved using a finite volume scheme. The results indicate that a low Prandtl number less than 0.7 had no effect of fluid flow intensity and heat transfer while the inclination angle had strong effect on it. The authors proposed important empirical equations of Nusselt number in terms of Prandtl number. Selimefendigil and Öztop [34] examined the mixed convection between circular cylinder within right-angled triangular enclosure heated partially from its left vertical wall. The governing equations had been solved numerically using a finite element method. The results are important because of increasing Hartmann number reduces both of entropy generation and heat transfer while increasing nanofluid volume fraction and speed of rotating circular cylinder increases both of them. Yu et al. [35] studied the unsteady free convection between circular cylinder within triangular enclosure under various effects of Grashof number, aspect ratio (inner diameter), and inclination angle. They simulated this phenomenon using CFD code ANSYS Fluent 6.3 which is based upon a finite volume method. They developed a relation between Nusselt number as a function of Grashof number for different inner cylinder diameters and inclination angles. Wang et al. [36] examined the mixed convection within the different sizes of an inner rotating circular cylinder located within a triangular enclosure and the gap between them was filled with Ethylene glycol-silicon carbide nanofluid for different Rayleigh numbers. Fluent CFD code had been used to simulate the whole of this problem. The results of this paper agreed with the previously published works. Sourtiji et al. [37] examined the natural fluid flow between a circular cylinder within a triangular nanofluid enclosure using a control volume based on a finite element scheme. The nanofluid thermal thermo-physical properties like viscosity and thermal conductivity had been predicted using Brinkman and Maxwell-Garnetts. It is obtained that adding void fraction of nanofluid had a remarkable impact at low Rayleigh numbers. Also, it had been observed that increasing inner circular cylinder diameter augments the heat transfer obviously. Another important investigation had been reported in Amrani et al. [38]. The authors studied the combined effect of radiation as well as free convective flow for triangular enclosure within rectangular body. As the most of researchers, finite volume method had been used to simulate this phenomenon under various Rayleigh numbers and aspect ratios.

#### 3. Trapezoidal

This section summarized the convection heat transfer due to the density difference between the inner body located within the trapezoidal enclosure [39-43]. Schematic representation of this case is presented in **Fig. 4**.



Hussein et al. [39] investigated numerically the mixed convection heat transfer between the inner circular rotating cylinder immersed in the trapezoidal enclosure using COMSOL which is based upon the finite element scheme. The gap between the inner body and the enclosure is divided into two layers system; the upper layer is filled with Copper-water nanofluid while the lower layer is consisting of the same nanofluid immersed in a saturated porous medium. The authors studied the influences of many dimensionless parameters such as Rayleigh and Darcy numbers, nanofluid void fraction as well as many geometrical parameters such as undulations number of a bottom wavy wall, inner body's diameter and rotational speed and the thickness of the porous layer. The results were crucial and indicated that the increasing of Rayleigh, Darcy numbers, nanofluid void fraction, and inner body's diameter rotational leads to augmentation in the local Nusselt number, and that means enhancement of the heat transfer. However the behavior of other parameters is inverse which means as the layer of the porous medium and the number of undulations goes up, the heat transfer is reduced. Esam et al. [40] examined the natural convection heat transfer in a trapezoidal enclosure filled with multilayers using the finite element method. The enclosure is partially heated from the bottom wall while the top wall is kept at isotherm cold temperature. The two inclined walls, as well as the inner circular cylinder and the rest length of the bottom wall, are assumed adiabatic. The upper layer is filled with Ag-water nanofluid, while the lower layer filled with

porous media saturated with the same nanofluid. The results had been validated with the previously published works and the agreement was good. The results indicate that increasing nanofluid, Darcy, and Rayleigh numbers increases the fluid flow intensity and the heat transfer rate. However, the behavior of porous layer thickness is completely reversed. Khan et al. [41] explained the mixed convection heat transfer between the inner heated circular cylinder rotating counter-clockwise located in a trapezoidal enclosure. The trapezoidal enclosure is kept adiabatic at its top and bottom wall while the two inclined walls are kept at cold temperatures. They made a comparison between the influence of the rotating cylinder and a motionless cylinder in a square enclosure. Their results confirmed that the rotating cylinder as well as the inclination angle of the sidewall effect significantly on the heat transfer. Selimefendigil [42] demonstrated numerically the natural convection between different shapes of the inner conductive body within a trapezoidal enclosure filled with different shapes of nanoparticle (blade, spherical, and cylindrical). The top and bottom walls are adiabatic while the left and right vertical walls are kept at isotherm hot and cold temperature respectively. The authors used finite element scheme to solve the governing equations and the validation seems good. The parameters of this study were Rayleigh number, thermal conductivity ratio, solid volume fraction, shapes of the nanoparticle and the inclination angle. It is worthy to mention that they conclude the shape of nanoparticle change obviously the heat transfer and the cylindrical shape is recommended for better Nusselt number and better enhancement in heat transfer. Ahmed et al. [43] visualized numerically using finite element techniques the heat lines in a nanofluid trapezoidal enclosure separated by a porous divider. The top wall is kept cold while a non-uniform temperature profile is applied to the bottom wall. The side walls are adiabatic. The parameters of this study are Rayleigh and Darcy number as well as nanofluid volume fraction as physical parameters. Also, many geometrical parameters had been investigated such as porous layer thickness and its positions as the authors moved it vertically upwards and downwards. The major findings were increasing the thickness of porous divider with the Rayleigh numbers augments the heat transfer. Also, the position of the porous divider is significant at low Rayleigh number while at higher Rayleigh number, the Nusselt number will be at the minimum values when the divider moved vertically downward.

We summarized the studies of the inner body within triangular and trapezoidal enclosure in **Table 4**.

| Table 4 | summarized | the studi | ies of nat | ural co | nvection | between | inner | bod | ly wit | hiı | n a | triangu | ar and | trapezoio | lal enc | closure |
|---------|------------|-----------|------------|---------|----------|---------|-------|-----|--------|-----|-----|---------|--------|-----------|---------|---------|
|---------|------------|-----------|------------|---------|----------|---------|-------|-----|--------|-----|-----|---------|--------|-----------|---------|---------|

| Ref                 | Objective             | Enclosure shape      | Software/  | Conclusions                           | Special findings                   |
|---------------------|-----------------------|----------------------|------------|---------------------------------------|------------------------------------|
|                     |                       |                      | model used |                                       |                                    |
| Xu et al. [32]      | Laminar free          | Cylinder inside      | CVM        | At constant aspect ratio, the         | Correlation of Nusselt number as a |
|                     | convection, effect of | triangular enclosure |            | inclination angle and Ra effect       | function of Ra for each value of   |
|                     | Ra, aspect ratio and  |                      |            | significantly on Nusselt number.      | aspect ratio                       |
|                     | inclination angle     |                      |            |                                       |                                    |
| Yu et al. [31]      | Effect of Prandtl     | Cylinder inside      | FVM        | Inclination angle had a strong        | Unique effect of low Prandtl       |
|                     | number                | coaxial triangular   |            | impact on Nu                          | number Nu while when Pr≥0.7 it     |
|                     |                       |                      |            |                                       | does not affect Nu                 |
| Selimefendigil and  | Mixed convection,     | Rotating insulated   | FEM        | Increasing nanofluid concentrations   | Hartmann number increasing leads   |
| Öztop [34]          | MHD, nanofluid,       | cylinder inside      |            | and rotating lead to an increasing in | to a reduction in both the entropy |
|                     | entropy               | triangular enclosure |            | total entropy and Nusselt number      | and Nusselt number                 |
| Yu et al. [35]      | Unsteady natural      | Cylinder inside      | ANSYS      | Correlations of Nusselt number had    | Nusselt number history had been    |
|                     | convection            | coaxial triangular   | Fluent     | been developed.                       | presented                          |
| Wang et al. Wang et | Mixed convection,     | Cylinder inside      | ANSYS      | Increasing Ra and nanofluid           | Rotational velocity effect         |
| al. [36]            | nanofluid             | coaxial triangular   | Fluent     | volume fraction improve the Nu        | significantly on Nu                |

| Sourtiji et al. [37] | Laminar buoyancy         | Cylinder inside       | CVFEM | Nanoparticle improve the heat as     | Maxwell-Garnetts (MG) and             |
|----------------------|--------------------------|-----------------------|-------|--------------------------------------|---------------------------------------|
|                      | driven flow, nanofluid   | triangular enclosure  |       | mentioned in most of the studies     | Brinkman models had been used to      |
|                      |                          |                       |       |                                      | simulate the nanofluid presence       |
| Amrani et al. [38]   | Radiation and natural    | Rectangle inside      | FVM   | Decreasing the aspect ratio and      | Thermal radiation promotes the heat   |
|                      | convection effect        | triangular enclosure  |       | increasing the Ra number enhances    | transfer                              |
|                      |                          |                       |       | the heat transfer                    |                                       |
| Hussein et al. [39]  | Mixed convection with    | Rotating cylinder in  | FEM   | The increasing the size and the      | Increasing porous thickness and       |
|                      | multi-layer system       | trapezoidal enclosure |       | rotation speed of the inner cylinder | number of undulation of the bottom    |
|                      |                          | with sinusoidal       |       | in addition to increases the Da, R   | wall reduce the heat transfer         |
|                      |                          | bottom wall           |       | and nanofluid loading will improve   |                                       |
|                      |                          |                       |       | the heat transfer                    |                                       |
| Esam et al. [40]     | free convection with     | Fixed adiabatic       | FEM   | The results indicate that increasing | Increasing porous thickness reduces   |
|                      | multi-layer system       | cylinder within       |       | Ra, Da and nanofluid loading         | the heat transfer                     |
|                      |                          | trapezoidal enclosure |       | enhance the heat transfer            |                                       |
| Khan et al. [41]     | Mixed convection, air    | Rotating cylinder in  | FEM   | Grashof number for large             | Rotating speed of the inner cylinder  |
|                      |                          | trapezoidal enclosure |       | inclination angle is very strong     | and inclination angle of the          |
|                      |                          |                       |       |                                      | trapezoidal wall effect highly on the |
|                      |                          |                       |       |                                      | Nusselt number                        |
| Selimefendigil [42]  | Natural convection       | Different shapes of   | FEM   | Effect of Ra, thermal conductivity   | Cylindrical nanoparticle gives better |
|                      | with different shapes of | inner body inside     |       | ratio, nanofluid loading and shapes  | performance                           |
|                      | nanoparticles (blades,   | trapezoidal           |       | of nanoparticle on Nu had been       |                                       |
|                      | spherical and            |                       |       | discussed                            |                                       |
|                      | cylindrical)             |                       |       |                                      |                                       |
| Ahmed et al. [43]    | Visualization of         | trapezoidal enclosure | FEM   | Increasing Ra, nanofluid volume      | Porous position equals to 0.5 gives   |
|                      | heatlines of free        | divided by porous     |       | fraction and Darcy number            | the better heat transfer              |
|                      | convection               | medium partition      |       | augments the heat transfer           |                                       |
|                      |                          |                       |       |                                      |                                       |

#### 4. Parallelogrammic

This section summarized the convection heat transfer due to the density difference between the inner body located within the parallelogrammic enclosure [44-48]. The computational domain of these shapes is inserted in **Fig. 5**.

Hussein [44] investigated numerically the influence of the position of an inner circular cylinder located inside a parallelogrammic enclosure filled with air using a finite volume method. The inner circular cylinder is kept at a hot temperature while both vertical walls are cold. The top and bottom walls are adiabatic. The effect of Rayleigh number, the inclination angle of the vertical wall, and the inner circular cylinder position had been taken into account and examined their effect on fluid flow strength and the heat transfer. It was obtained that the maximum flow strength will be when the inclination angle is zero i.e., for square enclosure when the cylinder moves upwards by +0.1. It was also obtained that when the cylinder moves downward will have greater Nusselt number than moving upwards. Majdi et al. [45] examined the natural convection between the hot circular cylinder immersed in a nanofluid parallelogrammic enclosure. The finite element had been used to solve the governing equations of heat transfer and fluid flow numerically. The validation was in good agreement with the previous publishing works. The results indicated that the increase of nanofluid volume fraction and Rayleigh number enhances the heat transfer especially if the inner circular cylinder moves vertically downwards until it reaches -0.1.

Chamkha [46] examined numerically the conjugate (conductive-natural and forced) convection within the parallelogrammic enclosure separated by solid partition using the finite volume method. The influence of various parameters such as Richardson number, the inclination angle of the enclosure from the cavity left vertical wall as well as the thermal conductivity ratio. The results were crucial and all of the mentioned parameters affect the heat transfer rate. Baïri [47] used a finite volume scheme to simulate free convection under transient conditions within a parallelogrammic enclosure filled with air. The enclosure is partially heated from its left vertical wall while cold temperature conditions are applied to the right wall. The top and bottom walls are kept adiabatic. Hussain et al. [48] simulated the free convection in a parallelogrammic enclosure containing a volumetric source under various inclination angles. The enclosure is heated non-uniformly from its left wall while the right wall is at isotherm cold temperature. The top and bottom walls are adiabatic.



Figure 5. Schematic diagram of the inner body in a parallelogrammic enclosure [45]

### 5. Rhombic

This section summarized the convection heat transfer due to the density difference between the inner body located within rhombic enclosure [49-53]. The present case is illustrated in **Fig. 6**.

Anandalakshmi and Basak [49] examined numerically the entropy generation and natural convection in a rhombic enclosure filled with saturated porous medium for different heating situation and inclination angle. Different uniform temperatures applied on the bottom and top walls where the bottom wall is warmer. Adiabatic conditions are considered to

both inclined vertical walls. The finite element scheme had been used to solve the continuity, momentum, and energy equations. Choi et al. [50] demonstrated the position of an inner circular cylinder located within the rhombic enclosure subjected to transient conditions using the immersed boundary scheme. The simulation of this study was done under various dimensionless parameters, which are Rayleigh number and inner cylinder locations, which is changed vertically upwards and downwards. The results indicated that when the cylinder moves up, two circulations formed below it, and the Rayleigh number had a significant effect on the maps of streamlines and isotherms. Another important study was presented by Hosseinjani and Nikfar [51] focused on the natural convective fluid flow between two horizontal circular cylinders located within the nanofluid rhombic enclosure. The impact of symmetry, asymmetry, instability, and stability of Cu-O nanofluid under various Rayleigh numbers had been explained. The impact of other parameters had been included such as diameter and the distance of inner cylinder, nanoparticle void fraction. The results reported that increasing the distance leads to an increase in transient asymmetric flow. Dogonchi et al. [53] investigated numerically the natural convection between the circular cylinder within a partially heated rhombic enclosure using CVFEM. The influence of nanoparticle shape factor, nanoparticle volume fraction, and had been examined. It is obtained the platelet shape had a better heat transfer rate.

The studies of the inner body within Parallelogrammic and Rhombic enclosure have been summarized in **Table 5**.





| Table 5 summarized the studies of natural | convection between in | ner body within | Parallelogrammic and Rhomb | oic enclosure |
|---|-----------------------|-----------------|----------------------------|---------------|
|   |                       |                 |                            |               |

| Ref                             | Objective  | Enclosure shape   | Software/  | Conclusions   | Special findings   |
|---------------------------------|--|---|------------|---|--|
|                                 |  |   | model used |   |  |
| Hussein [44]                    | Natural convection in<br>Parallelogrammic<br>enclosure for different<br>vertical locations                           | Cylinder inside<br>Parallelogrammic<br>enclosure filled<br>with air | FVM        | Increasing Ra leads to<br>enhance the heat transfer<br>and increases the fluid flow<br>strength. In addition, it is<br>recommended to incline the<br>vertical wall 15 for better                      | For better fluid flow strength and<br>heat transfer rate, it is<br>recommended to move the inner<br>cylinder towards the bottom wall<br>vertically   |
| Majdi et al. [45]               | Natural convection in<br>Parallelogrammic<br>enclosure for different   | Cylinder inside<br>Parallelogrammic<br>enclosure filled             | FEM        | fluid strength.<br>Ra and nanofluid enhance<br>the heat transfer and fluid<br>flow strength   | Increasing inclination angle<br>enhances the heat transfer   |
| Chamkha [46]                    | Mixed convection   | with nanofluid<br>Parallelogrammic<br>with solid partition          | FVM        | The Thermal conductivity<br>ratio, Ri number, inclination<br>angle and the direction of<br>movement of the left<br>vertical wall upward and<br>downward effect on heat<br>transfer and fluid dynamics | Mean skin friction coefficient<br>when the wall moves downward<br>was higher than if it moves<br>upward  |
| Baïri [47]                      | Unsteady buoyancy in<br>buildings  | Parallelogrammic<br>enclosure filled<br>with air                    | FVM        | The influence of Ra number<br>and the slop of the building<br>effect on the building<br>cooling   | The authors presented data for<br>analysis of building including<br>fluid flow and heat transfer   |
| Hussain et al.<br>[48]          | Free convection, heat<br>source with non-<br>uniform left sidewall   | Parallelogrammic<br>enclosure filled<br>with air                    | FVM        | Internal and external<br>Rayleigh number effect on<br>heat transfer.  | Increases inclination angle in<br>positive direction leads to a<br>reduction in fluid flow strength<br>while when it increases in the<br>negative direction; the fluid flow<br>circulation becomes larger. |
| Anandalakshmi<br>and Basak [49] | Free convective flow<br>with entropy<br>generation with two<br>different locations<br>(cases) of the heat<br>sources | Rhombic filled<br>with porous<br>medium                             | FEM        | Rhombic with inclination<br>angle 30 is recommended to<br>usage as it gives minimum<br>entropy generation.<br>However, it gives less heat<br>transfer enhancement                                     | Case 1 is better in energy<br>efficiency compared to case 2 as<br>the latter produces much<br>irreversibility more than case 1   |

| G1 1 1 1 1 5 0 1 | T C                    | D1 1 14           | TT 1) (  | I . D . I . I . I           | T. 1 1. 1 1.1 . 1.1             |
|------------------|------------------------|-------------------|----------|-----------------------------|---------------------------------|
| Choi et al. [50] | Impact of inner        | Rhombus with      | FVM      | Increasing Ra number leads  | It is obtained that minimum Nu  |
|                  | position of circular   | internal cylinder |          | to an augmentation in Nu    | is obtained when the cylinder   |
|                  | cylinder on heat       |                   |          |                             | moved upward. It is             |
|                  | transfer under         |                   |          |                             | recommended to move             |
|                  | transient state.       |                   |          |                             | downward for better heat        |
|                  |                        |                   |          |                             | transfer                        |
| Hosseinjani and  | Unsteady free          | Two-cylinder      | Immersed | At low Ra, the nanofluid    | The horizontal distance between |
| Nikfar [51]      | convection             | inside rhombic    | boundary | had a negligible effect on  | the circles effect on the       |
|                  |                        | enclosure         | scheme   | Nu. While at high Ra, Nu id | instability of the fluid flow   |
|                  |                        |                   |          | highly effected.            |                                 |
| Dogonchi et al.  | Nanoparticle shape     | Cylinder in       | CVFEM    | Rayleigh number and         | Platelet shape gives better     |
| [53]             | (platelet, cylindrical | partially thermal |          | nanofluid increasing helped | performance                     |
|                  | and spherical) effect  | active zone of    |          | in improving Nu             |                                 |
|                  | on heat transfer       | rhombus           |          |                             |                                 |

# 6. Elliptical

This section summarized the convection heat transfer due to the density difference between the inner body located within the elliptical enclosure [54-58] as shown in **Fig. 7**.

Sheikholeslami et al. [54] examined the natural convection between the inner elliptical body within a circular cylinder enclosure filled with nanofluid. The results explained that increasing Rayleigh number, nanoparticle, and inclination angle leads to an increase in the Nusselt number. Zhang et al. [55] investigated the natural convection between the hot elliptical inner body inside the cold square enclosure using a variational multiscale element scheme. The parameters were the major axis of the inner ellipse, Rayleigh number, and the inclination angle of the square enclosure. The results confirmed that inner body size, as well as the angle of inclination, had a noticeable impact on fluid flow. Sheikholeslami et al. [56] examined free convection, thermal radiation as well as a magnetic field between elliptical inner body within elliptical enclosure filled with nanofluid. Kefayati and Tang [57] examined numerically the inner cylinder or/and elliptical inner body inside a square enclosure by the lattice Boltzmann method. Abdulkadhim [58] demonstrated the free convection heat transfer within the elliptical enclosure with an inner circular cylinder. The gap was filled with nanofluid. The influence of the magnetic field, Rayleigh number, heat coefficient had been examined and addressed.



Figure 7. Schematic diagram of the inner body in an elliptical enclosure [56]

#### 7. Wavy enclosure

This section summarized the convection heat transfer due to the density difference between the inner body located within wavy enclosure [24, 52, 58-62]. As an illustrative example for this case is indicated in **Fig. 8**.



Figure 8. Schematic diagram of the inner body in an elliptical enclosure [62]

One of the interesting investigation that presented by Dogonchi [52] which concluded the inner rhombic body within wavy enclosure filled with Fe<sub>3</sub>O<sub>4</sub>. Control volume based upon the finite element method had been used in the simulation. Magnetic field dependent upon new viscosity model is employed. Many parameters had been included in the study like Rayleigh and Hartmann number, radiation parameters, aspect ratio, and nanoparticle shape factor (platelet, cylindrical, and spherical). The results highlighted that the increase of aspect ratio when the Hartmann number remains constant will reduce the rate of heat transfer. Jabbar et al. [59] examined the wavy interface on heat transfer between square enclosure divided into two layers, nanofluid/porous layer as well as a non-newtonian layer for various undulation number of wavy and Rayleigh numbers. Hatami and Safari [60] used the finite element method to solve the free convection between the circular cylinder inside the wavy nanofluid enclosure. Boulahia et al. [61] modeled the inner hot and cold cylinders inside the wavy enclosure. Abdulkadhim et al. [62] illustrated the multilayer system between the wavy inner cylinder within a wavy enclosure using a finite element scheme under various inner cylinder location and different undulations numbers. It can be seen in Table 6 which summarized the studies of elliptical and wavy enclosure with the internal body.

| Ref             | Objective             | Enclosure shape       | Software/  | Conclusions                   | Special findings                   |
|-----------------|-----------------------|-----------------------|------------|-------------------------------|------------------------------------|
|                 |                       |                       | model used |                               |                                    |
| Sheikholeslam   | Natural convection    | Circular enclosure    | CVFEM      | Increasing of nanofluid       | Increasing Ra reduces the          |
| i et al. [54]   | with nanofluid        | with inner elliptical |            | loading, Rayleigh number      | enhancement of heat transfer.      |
|                 |                       | body                  |            | and inclination angle         |                                    |
|                 |                       |                       |            | increases the Nusselt         |                                    |
|                 |                       |                       |            | number                        |                                    |
| Zhang et al.    | Natural convection    | Elliptical body       | FEM        | The size of inner ellipse, as | The effect of inclination angle is |
| [55]            |                       | inside tilted square  |            | well as Ra, is highly         | small on Nu                        |
|                 |                       | enclosure             |            | affected on Nu                |                                    |
| Sheikholeslam   | Natural convective    | Elliptical enclosure  | CVFEM      | Increasing of the inclination | Derivation of formula of Nu        |
| i et al. [56]   | flow, MHD, nanofluid  | with internal         |            | angle of the inner elliptical |                                    |
|                 |                       | elliptical body       |            | body increases the heat       |                                    |
|                 |                       |                       |            | transfer rate                 |                                    |
| Kefayati and    | Natural convection    | Circle and elliptical | LBM        | Increasing the size of        | As Bingham number goes up, heat    |
| Tang [57]       |                       | inner body inside     |            | cylinder augments the heat    | transfer goes down                 |
|                 |                       | square enclosure      |            | transfer                      |                                    |
| Abdulkadhim     | Natural convection,   | Circular body in a    | FEM        | Hartmann number and Ra        | The change of inner cylinder       |
| [58]            | MHD, heat             | nanofluid elliptical  |            | had an inverse effect on Nu   | horizontally effect on the heat    |
|                 | generation/absorption | enclosure             |            |                               | transfer characteristics           |
|                 | and nanofluid         |                       |            |                               |                                    |
| Jabbar et al.   | Free convection with  | Square enclosure      | FEM        | Nu decreases as the power     | Thickness layer effect on Nu       |
| [59]            | wavy wall             | with wavy wall        |            | index increases               |                                    |
| Hatami and      | Natural convection    | Internal cylinder     | FEM        | The location of inner         | The central location gives better  |
| Safari [60]     | and nanofluid         | inside wavy           |            | cylinder effect on heat       | heat transfer characteristics      |
|                 |                       | enclosure             |            | transfer                      |                                    |
| Boulahia et al. | Natural convection    | Cylinder inside       | FVM        | Ra and nanofluid increasing   | Increasing number of undulations   |
| [61]            |                       | wavy enclosure        |            | leads to increases the heat   | and reduction in the amplitude of  |
|                 |                       |                       |            | transfer                      | the wavy surface leads to          |
|                 |                       |                       |            |                               | augmentation in heat transfer      |
| Abdulkadhim     | Natural convection    | Wavy internal body    | COMSOL     | Number of corrugated effect   | The inner body position effect on  |
| et al. [62]     | with multilayer       | within wavy           |            | are small                     | heat and fluid flow                |
|                 | system                | enclosure             |            |                               |                                    |

Table 6 summarized the studies of natural convection between inner body within elliptical and wavy enclosure

# 8. Governing Equation

Finally, it is important to insert the governing equations used in this specific subject of natural convection heat transfer within enclosure filled with pure fluid, porous medium, and nanofluid [63].

8.1. Pure fluid

$$\frac{\partial U}{\partial x} + \frac{\partial V}{\partial Y} = 0 \tag{1}$$

$$U\frac{\partial U}{\partial x} + V\frac{\partial U}{\partial Y} = -\frac{\partial P}{\partial x} + Pr(\frac{\partial^2 U}{\partial x^2} + \frac{\partial^2 U}{\partial Y^2})$$
(2)

$$U\frac{\partial V}{\partial x} + V\frac{\partial V}{\partial Y} = -\frac{\partial P}{\partial Y} + Pr\left(\frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial Y^2}\right) + RaPr\theta$$
(3)

$$U\frac{\partial\theta}{\partial x} + V\frac{\partial\theta}{\partial Y} = \frac{\partial^2\theta}{\partial x^2} + \frac{\partial^2\theta}{\partial Y^2}$$
(40)

# 8.2. Porous Medium

$$\frac{\partial U}{\partial x} + \frac{\partial V}{\partial Y} = 0 \tag{5}$$

$$\frac{\partial U}{\partial Y} = -\frac{\kappa}{\mu} \frac{\partial^2 P}{\partial X \, \partial Y} \tag{6}$$

$$\frac{\partial V}{\partial x} = -\frac{\kappa}{\mu} \frac{\partial^2 p}{\partial x \, \partial y} + Ra \, \frac{\partial T}{\partial x} \tag{7}$$

$$U\frac{\partial\theta}{\partial x} + V\frac{\partial\theta}{\partial y} = \frac{\partial^2\theta}{\partial x^2} + \frac{\partial^2\theta}{\partial y^2}$$
(8)

8.3. Nanofluid

$$\frac{\partial U}{\partial X} + \frac{\partial V}{\partial Y} = 0 \tag{9}$$

$$\rho_{nf}\left(U\frac{\partial U}{\partial X} + V\frac{\partial U}{\partial Y}\right) = -\frac{\partial P}{\partial X} + \mu_{nf}\left(\frac{\partial^2 U}{\partial X^2} + \frac{\partial^2 U}{\partial Y^2}\right)$$
(10)

$$\rho_{nf}\left(U\frac{\partial U}{\partial X} + V\frac{\partial U}{\partial Y}\right) = -\frac{\partial P}{\partial Y} + \mu_{nf}\left(\frac{\partial^2 V}{\partial X^2} + \frac{\partial^2 V}{\partial Y^2}\right) \tag{11}$$

$$+g[(1-\varphi)(\rho\beta)_{bf}+\varphi(\rho\beta)_s](T-T_c)$$

$$U\frac{\partial\theta}{\partial x} + V\frac{\partial\theta}{\partial y} = \alpha_{nf} \left(\frac{\partial^2\theta}{\partial x^2} + \frac{\partial^2\theta}{\partial y^2}\right)$$
(12)

# 9. Conclusion

This paper presents a comprehensive literature review of the most published papers in the field of natural convection between inner bodies located inside different complex enclosure shapes. The main conclusions are:

- The inner bodies inside trapezoidal, parallelogrammic enclosure are very limited, and more investigation should be done.
- The studies regarding wavy enclosure are limited in a comparison with other simple shapes of enclosure despite its important applications is electronic equipment.
- There are limitations in the studies of natural convection between the inner body located in a wavy enclosure.
- Multi-layers system inside a wavy enclosure is limited as most of the recent studies focus on nanofluid, porous media filled the enclosure but there are serious limitations when the nanofluid/porous media filled the space.
- Dufour and Soret effect on natural flow for the multi-layer system are not investigated yet in full-details.

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