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# Indirect Electrochemical Oxidation of Phenol Using Rotating Cylinder Reactor

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#### Abstract

Indirect electrochemical oxidation of phenol and its derivatives was investigated by using MnO<sub>2</sub> rotating cylinder electrode. Taguchi experimental design method was employed to find the best conditions for the removal efficiency of phenol and its derivatives generated during the process. Two main parameters were investigated, current density (C.D.) and electrolysis time. The removal efficiency was considered as a response for the phenol and other organics removal. An orthogonal array  $L_{16}$ , the signal to noise (S/N) ratio, and the analysis of variance were used to test the effect of designated process factors and their levels on the performance of phenol and other organics removal efficiency. The results showed that the current density has the higher influence on performance of organics removal while the electrolysis time has the lower impact on the removal performance. Multiple regressions was utilized to acquire the equation that describes the process and the predicted equation has a correlation coefficient ( $\mathbb{R}^2$ ) equal to 98.77%. The best conditions were found to get higher removal efficiency. Removal efficiency higher than 95% can be obtained in the range of C.D. of 96-100 mA/cm<sup>2</sup> and electrolysis time of 3.2 to 5 h. The behavior of the chemical oxygen demand (COD) mineralization denotes to a zero order reaction and the rate of reaction controlled by active chlorine reaction not by mass transfer of phenol towards the anode.

**Key words:** Phenol removal, COD removal, manganese dioxide, rotating cylindrical electrode, Taguchi method.

#### Introduction

Petroleum refining is the chemical, physical, and thermal separation of crude oil into its main fractions and obtaining finished petroleum products through a series of separation and conversion steps. Petroleum refinery industry transforms crude oil into more than 2500 refined products, and large quantities of water are required for the purpose of attaining these products; about 80-90 % of the supplied water comes out as wastewater [1, 2].

The petroleum refinery wastewater is one of the worst contaminators of surface and ground waters and can cause detrimental environmental problems and tends to increase toxicity and creates the major environmental impact. In general, the effluent generated in the exploitation, production and refining of oil contains high concentrations of organic compounds with COD levels of approximately (300-600 ppm) and inorganic pollutants, sulphides, ammonia, chloride, 20-200 ppm of phenol, 1–100 ppm of benzene, heavy metals (0.1-100 ppm of chrome and 0.2–10 ppm of lead), suspended solids, grease and chemical additives. Consequently, these effluents need to be treated prior to discharge or reuse [3, 4].

Major consideration is paid to pollutants with an aromatic structure because they tend to be more toxic than their aliphatic complements. Aromatic compounds arise in many segments of the process industry, such as petroleum refineries, textiles, synthetic chemical plants, pulp and detergent, paper, plastics, pharmaceutical factories, pesticide, and herbicide. Water effluents containing aromatic chemicals are refractories, and are often toxic to biological Phenols treatment processes. are aromatic compounds enclosing one or more hydroxyl groups attached to the aromatic ring. Phenols are one of the widely distributed toxic substances and have been classified as one of the 65 priority pollutants which are considered to be harmful to humans and the environment and their presence must be limited to 0.1 mg/L [5-7].

Conventional wastewater treatment involves а series of mechanical, physical, chemical, and biological operations and processes, but these processes are not always preferred and have many limitations. technologies Electrochemical for removal of organics from petroleum refinery wastewater and wastewater of other industries have a great attention hence they offer many distinctive advantages relative to the other technologies such as; Compatibility Environment, Adaptability, with

Energy efficiency, Selectivity, Safety, Flexibility to automation, and Cost effectiveness [8, 9].

In electrochemical process, the destruction of organic pollutants may take place by either direct or indirect oxidation process. In the direct anodic oxidation process, the pollutants are first adsorbed on the anode surface and then removed by the anodic electron transfer reaction. It is well known that removal of phenol by direct electrochemical oxidation process causes a rapid fouling to the surface of employed electrode (such as graphite, platinum, ruthenium dioxide, lead dioxide, and tin dioxide) due to formation of a blocking polymer layer created by the polymerization of the phenoxy radicals produced in the initial stages of the reaction. This results in decreasing the active surface area of the electrode and a termination of the reaction within minutes [10]. In indirect oxidation process, strong oxidants such as hypochlorite/chlorine, hydrogen peroxide, ozone are electrochemically produced. The pollutants are then removed in the bulk solution by oxidation reaction of the produced oxidant. The effectiveness of the electrochemical oxidation process and its performance enhanced by the addition of high concentrations of chloride ions in water; beside it can decrease its energy consumption. All the oxidants are produced in situ and

immediately. are utilized The electrochemical method is one of the methods of oxidizing phenols which making it possible to attain an oxidant at the site of consumption and rapidly regulate the parameters of electrolysis. Since oxidation of phenol in the absence of mineral salts continues gently, the oxidizing process is conducted against the background of chlorides. The chief oxidizing agent in electro-oxidation in chloride solutions was activated chlorine formed in the water being treated as a result of anodic oxidation of chloride ions and subsequent chlorine hydrolysis. Activated chlorine presence speeds up the treatment process.

Sodium chloride (NaCl) is a very good choice hence it is easily available at reasonable cost, it is able to increase the electrical conductivity of the wastewater to a suitable level [11-13].

process During the of electrochemical oxidation of phenol, several aromatic and aliphatic intermediates are generated which they are more poisonous than phenol. Consequently, COD removal is very difficult in comparison with phenol removal because of the complex nature of COD and hence there are some intermediates can form, it is better to take the COD as a response as an alternative of phenol concentration. Moreover, longer electrolysis time is required for COD reduction compared phenol removal. The energy to consumption can be increased due to the extension of electrolysis time. So, the removal of organic contaminants in a very short time period makes the electrochemical method satisfactory for the industrial wastewater treatment applications. It can be concluded that electrochemical method an is successful for COD removal if it is successful for phenol removal, and vice versa [3, 14].

Most common anode materials used in wastewater treatment are graphite, lead/lead dioxide, nickel, platinum, SnO<sub>2</sub>-Sb, and boron doped diamond (BDD). These electrodes have some disadvantages, graphite is unstable or it could be oxidized to CO or CO<sub>2</sub>. Using PbO<sub>2</sub> electrode is not favorable due to the need for lead removal from the treated solution. SnO<sub>2</sub>-Sb electrode has problems with deactivation and short service life. High anodic stability and a wide potential window for water discharge are one of the most advantages of BDD; however, the limitation of using it efficiently for wastewater treatment is still restricted by its high cost, mechanical resistance problems and finding a suitable difficulties in substrate on which to deposit the thin diamond layer. The investigation of cheaper materials with analogous performances have attracted a great effort among these, manganese oxides  $(MnO_x)$ materials represent an attractive family for electrode manufacture, this is due to their unique electrochemical structures. good properties, good electrocatalytic properties, the relatively low cost, low environmentally toxicity. friendly character in comparison with other transition metal oxides, the natural abundance, and chemical stability [10, 13, 15].

The aim of the present study are applying galvanostatic conditions in the process of indirect electrochemical oxidation of phenol and its derivatives from a simulated wastewater and examining the performance of this batch electrochemical reactor by using the Taguchi method. The purposes of Taguchi approach were studying the effect of two parameters (C.D., and electrolysis time) on the removal efficiency using  $L_{16}$  orthogonal array experimental design, and determining the degree of significance of the factors on the removal studied efficiency using analysis of variance (ANOVA).

# **Experimental Work**

# 1. Materials and System

150 mg of phenol was dissolved in 1 L of distilled water for the preparation of simulated wastewater (which is equivalent to 315 mg/l of COD), and 1 g/l of NaCl, 0.1 M H<sub>2</sub>SO<sub>4</sub> (as a supporting electrolyte) added also, all chemicals used in experiments were of the reagent grade. The electrochemical cell consists of (2 liters) capacity glass reservoir fixed on plate magnetic stirrer a hot (LABINCO, model L-81), DC power supply (UNI-T: UTP3315TF-L) was used with outlet voltage (0-30 V) and output current (0-5 A). A cylindrical  $MnO_2$  on graphite substrate (with 30)  $cm^2$  as the effective area) was used as the anode. The cathode was a graphite hollow cylinder with inside an diameter of 8 cm and an outside

diameter of 10 cm and 15 cm length fixed in the glass electrolytic bath. The electrical connection of the rod was achieved by a cylindrical brass ring, and the rod insulated from the holder by a piece of Teflon. To rotate the anode with the required rotation speed, electrical stirrer an gear box (Heidolph) was used with electronic tachometer and the speed of rotation was 200 rpm. A schematic diagram of the electrochemical process is shown in Figure 1.



Fig. 1: schematic diagram of the electrochemical system

# 2. Procedure

- After the preparation of electrolytic solution, the cathode electrode which was the hallow cylinder graphite was dipped into the electrolytic solution, and the MnO<sub>2</sub> anode electrode was fixed to the agitator and dipped into the electrolytic solution.
- The electrodes were connected to the DC power supply and a constant current density was applied to the electrolytic cell for a specified time

and rotation speed of the electrical stirrer.

• The samples were collected during the electrolysis process, and the temperature of the electrolyte was maintained about  $25^{\circ}C \pm 1$ .

Taguchi design approach was used to study the effect of the two parameters on the removal efficiency of phenol and any other by products which was measured by the COD at the end of each experiment by using a COD reactor (Lovibond Water Testing, RD 125 model) where 2 ml of the sample was added to a vial containing a standard amount of a potassium dichromate oxidizing mixture. The phenol and any other organics exist in the sample would be oxidized for 2h at 150 °C. The vial was allowed to cool to room temperature and then a Photometer- System MD200 (Lovibond Water Testing) was used to measure the COD.

# 3. Taguchi Design

Full factorial design is a traditional optimization approach which involves a large number of experiments because it would take all possible combinations for studied variables. This approach is not useful because of time consuming and high operational cost [16].

Another method in the experimental design is called Taguchi method. Taguchi method can be used to determine the effect of factors on distinctive properties and the optimal conditions of the studied parameters. The determination of the possible combinations of factors and identification of best combinations can be easily achieved by this method [17, 18].

The Taguchi method uses a distinct design of orthogonal arrays. The Orthogonality means that factors can be evaluated individually from one another; the effect of one factor cannot be affected with the evaluation of the influence of another factor [19].

The variables considered for the study are time (t), and C.D. since they have a powerful effect on the performance of electro-oxidation process [20, 21], these variables and their levels are illustrated in Table 1, where four levels of each parameter were chosen. The suitable orthogonal array which allows the investigating of the effect of the considered parameters and the interaction between them for these levels would be  $L_{16}$ ; either (4<sup>2</sup>), and the experiments under the same conditions were carried out as shown in Table 1. Each row in this table represents one experimental run. The four values of time and C.D. were studied at four values (2, 3, 4, and 5 h) and (25, 50, 75, and 100 mA/cm<sup>2</sup>), respectively, corresponding to levels 1, 2, 3, and 4.

Table 1: Coded & real values of  $L_{16}$  orthogonal array

Exp. No.	Coded Values		Real Values		
	A	B	C.D. (mA/cm <sup>2</sup> )	Time (h)	
1	1	1	25	2	
2	1	2	25	3	
3	1	3	25	4	
4	1	4	25	5	
5	2	1	50	2	
6	2	2	50	3	
7	2	3	50	4	
8	2	4	50	5	
9	3	1	75	2	
10	3	2	75	3	
11	3	3	75	4	
12	3	4	75	5	
13	4	1	100	2	
14	4	2	100	3	
15	4	3	100	4	
16	4	4	100	5	

### **Results and Discussion**

Taguchi design of experiment (DOE) technique was applied at the present study to examine the most manipulating factors on COD removal efficiency, to find the best conditions of C.D., and time of electrolysis for organic pollutants removal. The  $L_{16}$  orthogonal array results illustrated in Table 2; the experimental data were analyzed using MINITAB 17 software.

Exp. No.	Real values		Response			
	$C.D.(mA/cm^2)$	Time(h)	COD(ppm)	Removal efficiency (%)	S/N	
1	25	2	290	7.9365	23.5461	
2	25	3	246	21.9048	27.3517	
3	25	4	188	40.3175	30.1682	
4	25	5	115	63.4921	31.9016	
5	50	2	236	25.0794	28.4772	
6	50	3	199	36.8254	32.2829	
7	50	4	122	61.2698	35.0994	
8	50	5	75	76.1905	36.8327	
9	75	2	154	51.1111	31.6877	
10	75	3	116	63.1746	35.4933	
11	75	4	88	72.0635	38.3098	
12	75	5	59	81.2698	40.0432	
13	100	2	58	81.5873	34.6706	
14	100	3	19	93.9683	38.4763	
15	100	4	5	98.4127	41.2928	
16	100	5	3.15	99.0000	43.0261	

Table 2: Results of experimental design for organics removal, \*COD initial value= 315 ppm

#### 1. Main Effect Plots

The relationship between the studied parameters and output response can be visualized by main effect plot. Figure 2 represents the Main effect plot for the COD removal efficiency (%) using indirect electrochemical oxidation process (i.e., electrooxidation of organics in the presence of NaCl), where 1 g/l of NaCl was added to the electrolytic solution. It is well-known that the phenol removal is achieved by the reactive chlorine species such as chlorine and hypochlorous acid or hypochlorite ion (Cl<sub>2</sub>, HOCl and OCl<sup>-</sup>) that react very fast with organics chiefly by the reactions in solution. Free chlorine is the dominant oxidizing agent in acidic conditions, while in slightly alkaline conditions hypochlorite, chloride ions and hydroxyl radicals are all produced in appropriate concentrations [22]. The HOCl generation increases as the C.D. also increases, therefore the organic removal efficiency increased. The organic removal also governed by the electrolysis time, the generation of HOCl increases with time increasing.

# 2. Signal –to- Noise

A basic signal- to-noise (S/N) ratio is a quantitative measure that employed by Taguchi method to determine the optimum removal conditions, besides it used for the evaluation of the variation of the response around the mean value due to experimental noise, so an optimal response with smaller variations can be obtained. The terms 'signal' to 'noise' ratio signify the desirable (mean for output characteristic) the and undesirable values (standard deviation (SD) for the output characteristic) for the output response, respectively. The analysis of means and S/N ratio that recommended by Taguchi uses a approach theoretical that includes plotting the effects and visually recognizing the factors that appear to be significant, without the need for ANOVA analysis, so the analysis would be very simple [23, 24].

The choice principles of S/N ratio depend on the objective of the design; The S/N ratios are different according to the type of output response. Generally, a better signal attained when the noise is smaller, so that a larger S/N ratio yields better results. Therefore, the optimal level of process parameters is the level with the highest S/N ratio. Usually, there are three types of S/N ratios, higher is best (HB), nominal-is-best (NB), and lower is best (LB) to choose from. For each level of the process parameters, the S/N ratio computed based on the S/N analysis [25].



Fig. 2: Main effect plot for organics removal efficiency

In order to maximize the removal efficiency the bigger is better approach is implemented, in which the S/N ratio is calculated as presented in Equation 1 [26]:

$$S/_{N} = -10 \log \left[\frac{1}{n} \left(\sum_{i=1}^{n} \frac{1}{y_{i}^{2}}\right)\right] \dots (1)$$

Where  $y_i$  is the response of each experiment, and n is the repetition number of each experiment.

S/N ratio can reflect both the average and the variation of the quality characteristics; so, it merges several repetitions into one value which reflects the amount of variation present [16].

Table 2 shows the S/N ratios calculated based on Equation 1 for all the responses of experiments.

The effect of each control parameter on the response obtained from the response Table 3 for S/N

which represented graphically in Figure 3. This table contains ranks delta which based on statistics. compare the relative magnitude of effects. The highest average for each factor minus the lowest average for the same called the delta statistics. Rank 1 is assigned to the highest delta value, rank 2 to the second highest delta value; and so on, so ranks are assigned based on delta values [27]. Therefore, the values of delta in this table indicate that the current density has the greatest influence on the organic removal followed by time, and speed of rotation.

In the main effect plot of S/N ratio, the x-axis point to the value of each process parameter at three levels and the y-axis is the response S/N values. The main effect plots used to determine the optimum conditions of the design, so obtaining the optimal value of the responses.

According to the main effect plot of S/N ratio, the best conditions for the organic removal are current density of  $100 \text{ mA/cm}^2$ , and electrolysis time of 5 h. These conditions are the conditions

of run (16), so no confirmation step is required in this analysis. The COD removal efficiency was 99 %.

Level	C.D.	Time
1	28.24	29.60
2	33.17	33.40
3	36.38	36.22
4	39.37	37.95
Delta	11.12	8.36
Rank	1	2



Table 3: Response Table for Signal to Noise Ratios (bigger is better)

#### **3.** Analysis of Variance (ANOVA)

The utilization of ANOVA by Taguchi method is a very good implement to find out which are statistically the most significant parameter and to find out the value of percentage contribution of each factor to a change in the dependent variable. Analysis of variance on the experimental results accomplished to determine the variation source during the process of indirect electrochemical oxidation of the organics; then the identification of the effect order of factors on the organics removal would relatively be easy [28].

The ANOVA was established based on the degree of freedom (DF),

the sum of the square (SS), the percentage contribution of each parameter, adjusted sum of squares (Adj SS), adjusted mean of square (Adj MS), F-value, and P-value. The statistical expressions of these terms can be defined in many books and studies dealing with experiments design and analysis [29].

Any factor has a high percent contribution; then a small variation in its magnitude will have a great influence on the performance. The percentage contribution for each parameter defied as the portion of a total observed variance in the experiment for each significant parameter. When the value of this

Fig. 3: Main effect plots of SN ratios for removal efficiency of phenol and other organics

percentage contribution is greater, then it contributes to the final results more than other factors [26].

The results of the ANOVA summarized in Table 4. As in the S/N ratio analysis, it is obvious that the significance of the factors succeeds in the following order of importance: C.D.> electrolysis time.

The data given in Table 4 showed that the contributions of the two factors i.e. C.D., and time of electrolysis were 66.03 and 28.37%, respectively. It is clear that current density has the greatest contribution on organic removal followed by electrolysis time.

Statistically, the F value for each studied parameter is the ratio of the mean of squared deviations to the mean of squared error. For the present condition, the value of  $F_{(1, 15)}$  with 95% confidence level is 4.2417 [30]. Generally, when F>4, it means that the studied parameter is significant and the variation of it makes a big change on the performance [18].

It is obvious from the results of F value in Table 4 that all the two studied parameters are significant since all of them have F > 4.

The significance of each factor on response is determined by P-value. If p-value value < 0.05 (for a confidence level of 95%) indicates that the factor is significant. P-values in this study < 0.05 (for a confidence level of 95%); indicate that all model terms are significant.

Measuring the proportion of the total variability explained by the model is called the  $R^2$  static, is close to (1) for our response. The same result acquired with respect to the adjusted  $R^2$ , which used for considering the model significance since it is convenient when comparing the model with different number of terms. The results illustrate that adj. $R^2$  is not suggestively different from the ordinary  $R^2$ .

Residual plots used to calculate the adequacy of the model. The residual plots for phenol and other organic removal are presented in Figure 4.

The descriptions of each residual plot for the present experiments known as followed:

- Normal probability plot point out that the data are normally distributed and the variables are manipulating the response. There are no Outliers existing in the data.
- Histogram proves that the data are not skewed and no outliers exist.
- Residuals versus fitted values indicate that the variance is constant and a non-linear relationship exists. Ideally, the points should fall randomly on both sides of zero.
- Residuals versus order of the data indicate that there are systematic effects in the data due to time or data collection order.

Source	DF	Seq SS	Contribution	Adj SS	Adj MS	F- Value	P- Value
C.D.	3	7839.6	66.03%	7839.6	2613.20	35.35	0.000
Time	3	3368.7	28.37%	3368.7	1122.89	15.19	0.001
Error	9	665.3	5.60%	665.3	73.92	-	-
Total	15	11873.6	100.00%	-	-	-	-
General Linear Model	S 8.59764	R-sq 94.40%	R-sq(adj) 90.66%	PRESS 2102.60	R- sq(pred) 89.29%	-	-

Table 4: Analysis of Variance for organic removal efficiency

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Fig. 4: Residual plots of organics removal efficiency

#### 4. Multiple Regression Analysis

The multiple regression model for COD removal efficiency is as follows:

 $\begin{array}{l} COD \ removal\% = -61.87 + \\ 0.940 \ X_1 + 24.56 \ X_2 + 0.0039 \ X_1^2 - \\ 0.1854 \ X_1. X_2 \qquad \qquad \dots (2) \end{array}$ 

Where  $X_1$  is current density and  $X_2$  is electrolysis time. The predicted equation had the squared value of the

correlation coefficient ( $\mathbb{R}^2$ ) equal to 98.77% with error percentage equal to 2 %.

Contour plot presented in Figure 5 clarifies that the best conditions for getting removal efficiency > 95% are C.D. within the range 96-100 mA/cm<sup>2</sup>, and time of 3.2-5 h. Using 100 mA/cm<sup>2</sup> gives removal efficiency > 95% within 3.2 h, while using 90 mA/cm<sup>2</sup> gives it within 5h.



Fig. 5: Contour Plot of removal efficiency versus C.D. (mA/cm<sup>2</sup>) and Time (h)

The decay in COD affected intensely by the concentration of chloride ion (Cl<sup>-</sup>) and by the operational variables (current and voltage). The effects of current densities on COD are presented in Figure 6. Phenol removal succeeded by the reactive chlorine species (i.e., hypochlorous acid (HOCl)), which is the dominant oxidizing agent in acidic conditions. The COD decreased and removal percentage increased with the C.D. increasing. As the C.D. increases from 30 to 90 mA/cm<sup>2</sup>, the COD decreases linearly from 315 to 110.61, and 18.34 ppm, respectively. While the removal efficiency increases from 64.88 to 94.17 % respectively. The linear behavior of the COD reduction under different current densities refers to a zero order reaction and the rate of reaction controlled by active chlorine reaction not by mass transfer of phenol towards the anode. These results are in agreement with previous studies done by other workers [15, 21, 31].



Fig. 6: COD vs. electrolysis time at different current densities for rotating  $MnO_2$  cylinder electrode, COD<sub>0</sub>=315 ppm

### Conclusion

Removal of phenol has been studied in the present work by indirect electrochemical oxidation and a DOEs (derived from the Taguchi approach technique) was applied to observe the best experimental conditions, C.D. and designated as the studied time parameters, and these factors varied at four levels with an orthogonal array of  $L_{16}$ , which could examined with the bigger is better as a quality character. Taguchi analysis suggested that C.D. has the largest influence on the of performance electrochemical removal of phenol and other organics. Based on The results of the ANOVA, it can be established that the significance of the factors has the

following order of importance: C.D. followed by the electrolysis time. Based on Taguchi multiple regression model, the best conditions for removal efficiency of COD equal to 99%, were C.D. of 100 mA/cm<sup>2</sup> and electrolysis time of 5 h.

#### References

- I. D. Santos, M. Dezotti, and A. J. B. Dutra, "Electrochemical treatment of effluents from petroleum industry using a Ti/RuO<sub>2</sub> anode,," *Chem. Eng. J.*, vol. 226, pp. 293–299, 2013.
- 2. N. V. Fomchenko, I. N. Shcheblykin, and V. V. Biryukov, "Cleaning Concentrated Refinery Wastewaters From Sulfides, Phenols, And Ammonia

Nitrogen,"*Chem. Pet. Eng.*, vol. 35, no. 7, pp. 399–402, 1999.

- 3. Y. Yavuz, A. S. Koparal, and Ü. Bak, "Treatment of petroleum refinery wastewater by electrochemical methods," *Desalination*, vol. 258, pp. 201– 205, 2010.
- D. S. Ibrahim, P. S. Devi, and N. Balasubramanian, "Electrochemical Oxidation Treatment of Petroleum Refinery Effluent," *Int. J. Sci. Eng. Res.*, vol. 4, no. 8, pp. 1–5, 2013.
- S. Randazzo, O. Scialdone, E. Brillas, and I. Sirés, "Comparative electrochemical treatments of two chlorinated aliphatic hydrocarbons. Time course of the main reaction by-products," *J. Hazard. Mater.*, vol. 192, no. 3, pp. 1555–1564, 2011.
- X. Y. Li, Y. H. Cui, Y. J. Feng, Z. M. Xie, and J. D. Gu, "Reaction pathways and mechanisms of the electrochemical degradation of phenol on different electrodes," *Water Res.*, vol. 39, no. 10, pp. 1972–1981, 2005.
- V. Smith De Sucre And A. P.Watkinson, "Anodic Oxidation of Phenol for Waste Water Treatment," *Can. J. Chem. Eng.*, vol. 59, pp. 52–59, 1981.
- A. A. Batoeva, M. R. Sizykh, A. A. Ryazantsev, M. S. Khandarkhaeva, and D. G. Aseev, "Electrochemical Oxidation of Phenols," *Russ. J. Appl. Chem.*, vol. 80, no. 8, pp. 1365–1368, 2007.
- K. Rajeshwar and J. G. Ibanez, *Environmental Electrochemistry: Fundamentals and Applications in Pollution Sensors*, no. May. Elsevier Science & Technology Books, 1997.
- P. L. Hagans, P. M. Natishan, B. R. Stoner, and W. E. O'Grady, "Electrochemical oxidation of phenol using boron-doped diamond electrodes," *J. Electrochem. Soc.*,

vol. 148, no. 7, pp. E298–E301, 2001.

- Κ. Chandra 11. K. S. Vimal Digvijay Patil. Srivastava, "Parameteric Optimization of Dye by Electrocoagulation Removal Using Taguchi Methodology," Int. J. Chem. React. Eng., vol. 9, no. A8, pp. 1–19, 2011.
- S. Y. Bashtan and V. A. Bagrii, "Electrochemical Oxidation of Phenol on Metaloxide Electrodes," *J. Water Chem. Technol.*, vol. 34, no. 1, pp. 24–27, 2012.
- 13. D. Rajkumar, J. G. Kim, and K. Palanivelu, "Indirect electrochemical oxidation of phenol in the presence of chloride for wastewater treatment," *Chem. Eng. Technol.*, vol. 28, no. 1, pp. 98–105, 2005.
- 14. Y. Yavuz and A. S. Koparal, "Electrochemical oxidation of phenol in a parallel plate reactor using ruthenium mixed metal oxide electrode," *Journal of Hazardous Materials*, vol. 136, no. 2. pp. 296– 302, 2006.
- 15. P. H. Britto- Costa and L. A. M. Ruotolo, "Phenol Removal From Wastewaters By Electrochemical Oxidation Using Boron Doped Diamond (Bdd) And Ti/Ti<sub>0.7</sub>Ru<sub>0.3</sub>O<sub>2</sub>," *Brazilian J. Chem. Eng.*, vol. 29, no. 04, pp. 763–773, 2012.
- 16. Y. Ma, H. Hu, D. Northwood, and X. Nie, "Optimization of the electrolytic plasma oxidation processes for corrosion protection of magnesium alloy AM50 using the Taguchi method," *J. Mater. Process. Technol.*, vol. 182, no. 1– 3, pp. 58–64, 2007.
- 17. K. Do Kim, D. N. Han, and H. T. Kim, "Optimization of experimental conditions based on the Taguchi robust design for the formation of nano-sized silver particles by chemical reduction method," *Chem.*

*Eng. J.*, vol. 104, no. 1–3, pp. 55–61, 2004.

- G. Barman, A. Kumar, and P. Khare, "Removal of congo red by carbonized low-cost adsorbents: Process parameter optimization using a Taguchi experimental design," *J. Chem. Eng. Data*, vol. 56, no. 11, pp. 4102–4108, 2011.
- 19. Y.-C. Chen, P.-J. Tsai, and J. Mou, "Determining Optimal Operation Parameters for Reducing PCDD / F Emissions (I-TEQ values) from the Iron Ore Sintering Process by Using the Taguchi Experimental Design," *Environ. Sci. Technol.*, vol. 42, no. 14, pp. 5298–5303, 2008.
- P. H. Britto-costa, R. B. Alencarsouza, and L. A. M. Ruotolo, "Electrochemical degradation of phenol at BDD anodes in chloride medium," pp. 1–8.
- Z. Tasic, V. K. Gupta, and T. F. Bor, "The Mechanism and Kinetics of Degradation of Phenolics in Wastewaters Using Electrochemical Oxidation," *Int. J. Electrochem. Sci.*, vol. 9, pp. 3473–3490, 2014.
- 22. J. Pires, D. P. Barreto, E. Vieira, M. M. Oliveira, D. Ribeiro, J. F. De Souza, and C. A. Martínez-Huitle, "Electrochemical mediated oxidation of phenol using Ti/IrO<sub>2</sub> and Ti/Pt-SnO<sub>2</sub>-Sb<sub>2</sub>O<sub>5</sub> electrodes,"*J. Electrochem. Sci. Eng.*, vol. 4, no. 4, pp. 259–270, 2014.
- 23. Y. Q. Wang, J. H. Byun, B. S. Kim, J. Il Song, and T. W. Chou, "The use of Taguchi optimization in determining optimum electrophoretic conditions for the deposition of carbon nanofiber on carbon fibers for use in carbon/epoxy composites," *Carbon N. Y.*, vol. 50, no. 8, pp. 2853–2859, 2012.
- M. Vega, R. Pardo, E. Barrado,M. A. de la Fuente, and J. L. delValle, "Application of the taguchi

experimental design to the optimisation of a photo-oxidation procedure for trace metal analysis in freshwater," *Fresenius. J. Anal. Chem.*, vol. 350, no. 3, pp. 139–144, 1994.

- J. F. Martínez-Villafañe and C. Montero-Ocampo, "Optimisation of energy consumption in arsenic electro-removal from groundwater by the Taguchi method," *Sep. Purif. Technol.*, vol. 70, no. 3, pp. 302– 305, 2010.
- 26. A. Zirehpour, A. Rahimpour, M. Jahanshahi, and M. Peyravi, "Mixed matrix membrane application for olive oil wastewater treatment: Process optimization based on Taguchi design method," *J. Environ. Manage.*, vol. 132, pp. 113–120, 2014.
- 27. H. Ashassi-Sorkhabi and R. Bagheri, "Sonoelectrochemical synthesis, optimized by Taguchi method, and corrosion behavior of polypyrrole-silicon nitride nanocomposite on St-12 steel," *Synth. Met.*, vol. 195, pp. 1–8, 2014.
- 28. Y. G. Adewuyi and B. A. Oyenekan, "Optimization of a sonochemical process using a novel reactor and Taguchi statistical experimental design methodology," *Ind. Eng. Chem. Res.*, vol. 46, no. 2, pp. 411–420, 2007.
- 29. Y. W. Genichi Taguchi, Subir Chowdhury, *Taguchi's Quality Engineering Handbook*. 2005.
- 30. R. K. Roy, *A Primer on TheTaguchi Method*, 2nd editio. Society of Manufacturing Engineers, 2010.
- 31. B. K. Krbaht, B. Salih, and A. Tanyolac, "Electrochemical conversion of phenolic wastewater on carbon electrodes in the presence of NaCl," *Journal of Chemical Technology and Biotechnology*, vol. 77, no. 1. pp. 70–76, 2002.